Appendix 1.33. Model Archive Summary for Suspended-Sediment Concentration at U.S. Geological Survey site 07143672; Little Arkansas River at Highway 50 near Halstead, Kansas, during March 2017 through October 2019

This model archive summary summarizes the suspended-sediment concentration model developed to compute hourly or daily suspended-sediment concentration. Model development methods follow U.S. Geological Survey (USGS) guidance from Office of Surface Water/Office of Water Quality Technical Memoranda and USGS Techniques and Methods, book 3, chap. C4 (Rasmussen and others, 2009).

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Site and Model Information

Site Number: 07143672

Site Name: Little Arkansas River at Highway 50 near Halstead, Kansas

Location: Latitude 38°01'43", longitude 97°32'25" referenced to North American Datum of 1927, in NW 1/4 NE 1/4 NE 1/4 sec.28, T.23 S., R.2 W., Harvey County, Kansas, hydrologic unit 11030012.

Equipment: A Sutron Satlink II High Data Rate Collection Platform and a Design Analysis Water Log H350/355 nonsubmersible pressure transducer transfers real-time stage and water-quality data via satellite. The primary reference gage is a Type-A wire-weight gage located on the downstream bridge guardrail. Check-bar elevation is 33.396 feet. The orifice tube is enclosed in 1.25-inch steel conduit trenched into the ground down to the edge of water, where the orifice emerges from the bank and culminates in a 2-inch open-end orifice tethered to a steel fencepost near the left edge of water. Gage height was measured during May 1998 through December 2019. A YSI 6600 water-quality monitor equipped with water temperature, specific conductance, pH, dissolved oxygen, and turbidity (a YSI Model 6026 [December 1998 through December 2006] and YSI Model 6136 [July 2004 through December 2017]) sensors collected data during May 1998 through December 2017] sensors collected data during May 1998 through December 2017]. A YSI EXO2 water-quality monitor equipped with water temperature, specific conductance, pH, dissolved organic matter sensors collected data during January 2017 through December 2019. A Hach Nitratax monitor collected nitrate data during February 2017 through December 2019.

Date model was developed: June 1, 2020

Model calibration data period: March 30, 2017 through October 8, 2019

Model Data

All data were collected using USGS protocols (U.S. Geological Survey, variously dated; Wagner and others, 2006; Sauer and Turnipseed, 2010; Turnipseed and Sauer, 2010) and are stored in the National Water Information System (NWIS) database (U.S. Geological Survey, 2021). Explanatory variables were evaluated individually and in combination. Potential explanatory variables included streamflow, water temperature, specific conductance, pH, dissolved oxygen, YSI EXO2 turbidity, nitrate, and fluorescent dissolved organic matter. Seasonal components (sine and cosine variables) also were evaluated as explanatory variables.

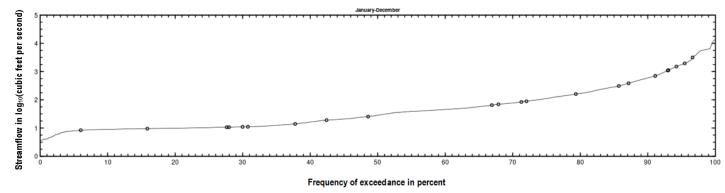
The regression model is based on 22 concomitant values of discretely collected suspended-sediment concentration and continuously measured turbidity during March 2017 through October 2019. Discrete samples were collected over a range of streamflow and turbidity conditions. No samples had concentrations that were below laboratory detection limits. Summary statistics and the complete model-calibration dataset are provided below. Outliers and influential points were identified using studentized residuals, DFITS, Cook's D (Cook, 1977), and leverage. Outliers in previously published versions of this model (Christensen and others, 2003; Rasmussen and others, 2016) were examined and retained in the dataset if there were no clear issues, explanations, or conditions that would cause a result to be invalid for model calibration. Two samples (collection dates January 30, 2018 and December 10, 2019) were not representative of the dataset and exceeded Cook's D and DFITS outlier criteria and were removed from the model dataset to avoid erroneous inflation of model-computed values at the upper range of surrogate relations. Removing data points based only on outlier

criteria may only overestimate the certainty of the model.

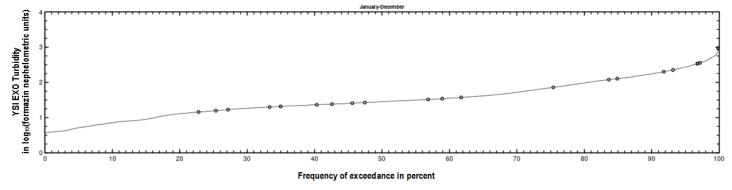
Suspended-Sediment Concentration

Discrete samples were collected from the downstream side of the bridge or instream within 50 feet of the bridge using equal-width-increment, multi-vertical, single vertical or grab-dip methods following U.S. Geological Survey (variously dated) and Rasmussen and others (2014). Discrete samples were collected on a semifixed to event-based schedule ranging from 6 to 9 samples per year with a FISP US DH–95 or D–95 with a Teflon bottle, cap, and nozzle depth-integrating sampler, a DH–81 with a Teflon bottle, cap, and nozzle hand sampler or a grab sample with a Teflon bottle depending on sample location. Samples were analyzed for suspended-solids concentration by the USGS Iowa Sediment Laboratory following standard methods (Guy, 1969).

Suspended-Sediment Concentration Samples Plotted on Streamflow Duration Curve



Suspended-Sediment Concentration Samples Plotted on YSI EXO Turbidity Duration Curve



Continuous Data

Concomitant turbidity values were time interpolated. If no concomitant continuous data were available within 2 hours of sample collection, the sample was not included in the dataset.

Model Development

Ordinary least squares regression analysis was done using R (version 4.0.0) programming language (R Core Team, 2020) to relate discretely collected suspended-solids concentration to turbidity and other continuously measured data. The distribution of residuals was examined for normality and plots of residuals (the difference between the measured and model-calculated values) compared to model-computed suspended-solids concentration were examined for homoscedasticity (departures from zero did not change substantially over the range of model-calculated values). Previously published explanatory variables were also strongly considered for continuity; however, the best explanatory variable(s) were ultimately selected.

Turbidity was selected as the best predictor of suspended-sediment concentration based on residual plots, high coefficient of determination (R^2), and low model standard percentage error (MSPE). Turbidity was positively correlated with total suspended solids because turbidity measures light scattered by particulates in water.

Model Summary

Summary of final suspended-solids concentration regression analysis at USGS site number 07143672:

Suspended-solids concentration-based model:

$$\log_{10}(SSC) = 1.1 \times \log_{10}(TBY) + 0.143$$

where,

 $log_{10} = logarithm$ base 10; SSC = suspended-sediment concentration, in milligrams per liter (mg/L); and TBY = turbidity, in formazin nephelometric units (FNU)

The log-transformed model may be retransformed to original units so that SSC can be calculated directly. The retransformation introduces a bias in the calculated constituent. This bias may be corrected using Duan's bias correction factor (BCF; Duan, 1983). For this model, the calculated BCF is 1.02. The retransformed model, accounting for BCF is:

 $SSC = 1.418 \times TBY^{1.1}$

Model Statistics, Data, and Plots

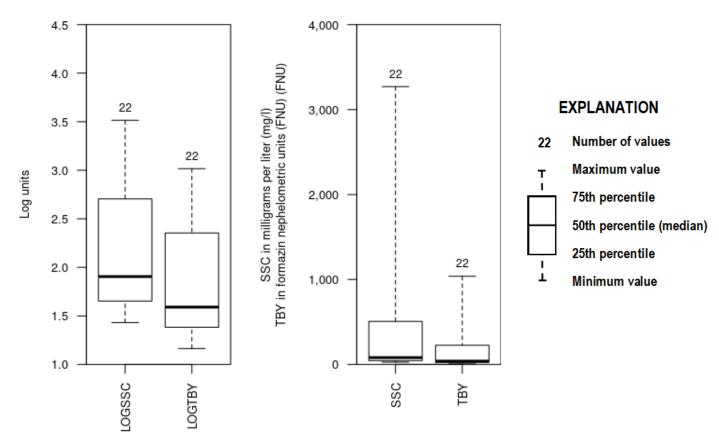
Model

LOGSSC = + 1.1 * LOGTBY + 0.143

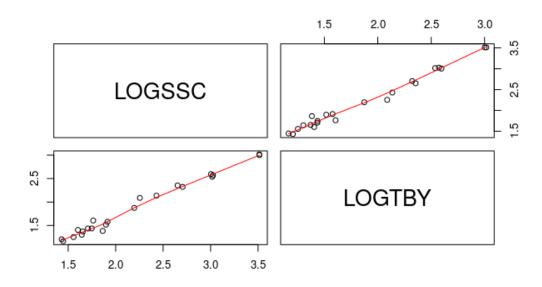
Variable Summary Statistics

	,			
	LOGSSC	SSC	LOGTBY	TBY
Minimum	1.43	27.0	1.16	14.6
1st Quartile	1.65	45.0	1.38	24.2
Median	1.91	80.5	1.59	39.0
Mean	2.21	537.0	1.87	192.0
3rd Quartile	2.71	507.0	2.35	226.0
Maximum	3.51	3270.0	3.02	1040.0





Exploratory Plots



Basic Model Statistics

Number of Observations	22
Standard error (RMSE)	0.0855
Average Model standard percentage error (MSPE)	19.8
Coefficient of determination (R ²)	0.984
Adjusted Coefficient of Determination (Adj. R ²)	0.984
Bias Correction Factor (BCF)	1.02

Explanatory Variables

	Coefficients	Standard Error	t value	Pr(> t)
(Intercept)	0.143	0.0607	2.36	2.85e-02
LOGTBY	1.100	0.0310	35.60	1.44e-19

Correlation Matrix

	Intercept	E.vars
Intercept	1.000	-0.954
E.vars	-0.954	1.000

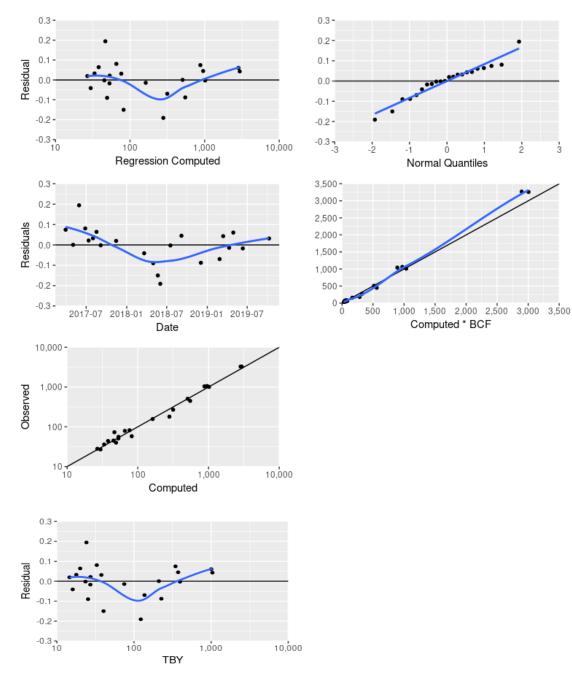
Outlier Test Criteria

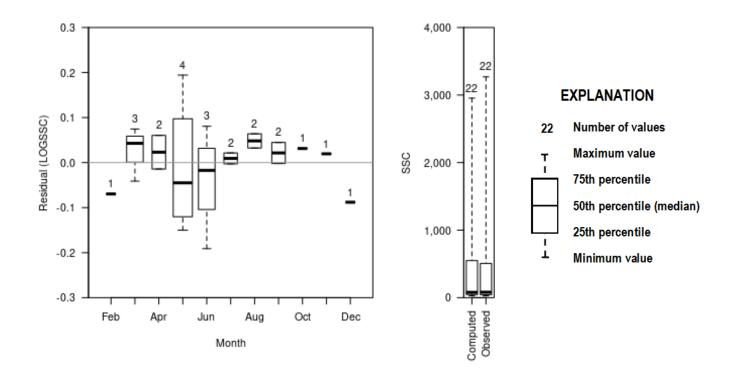
Leverage Cook's D DFFITS 0.273 0.193 0.603

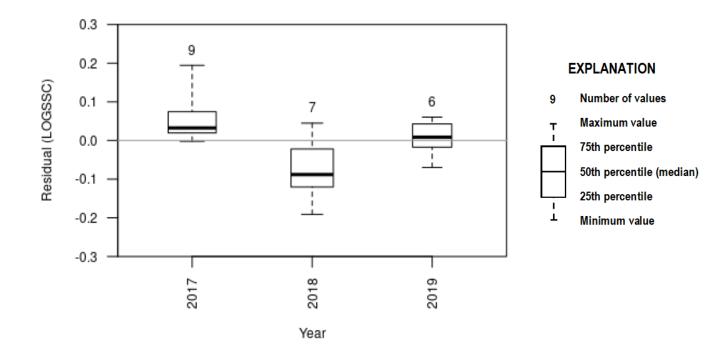
Flagged Observations

	LOGSSC	Estimate	Residual	Standard	Studentized	Leverage	Cook's	DFFITS
				Residual	Residual		D	
5/30/2017 12:10	1.86	1.67	0.194	2.36	2.72	0.0766	0.232	0.782
6/2/2018 9:20	2.26	2.45	-0.191	-2.29	-2.6	0.0517	0.143	-0.608

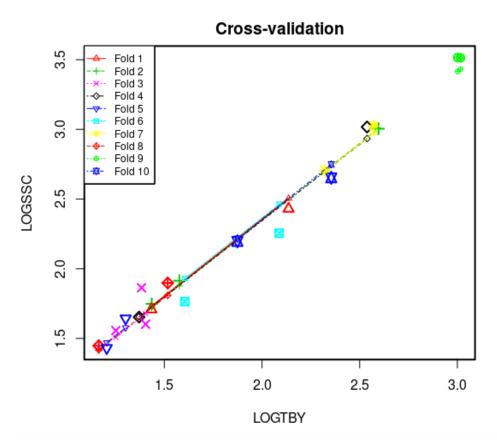
Statistical Plots



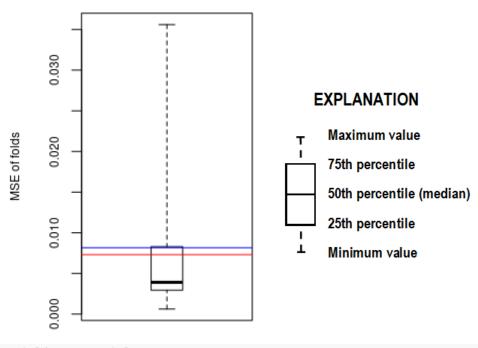




Cross Validation



Minimum MSE of folds: 0.000622 Mean MSE of folds: 0.008160 Median MSE of folds: 0.003910 Maximum MSE of folds: 0.035600 (Mean MSE of folds) / (Model MSE): 1.120000



Red line - Model MSE

Blue line - Mean MSE of folds

Model-Calibration Dataset

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	Date	LOGSSC	LOGTBY	SSC	ТВҮ	Computed LOGSSC	Computed SSC	Residual	Normal Quantiles
1	3/30/2017	3.02	2.54	1040	345	2.94	891	0.0745	1.19
2	5/3/2017	2.71	2.32	507	210	2.7	516	0.000267	-0.0565
3	5/30/2017	1.86	1.38	73	24.2	1.67	47.5	0.194	1.93
4	6/27/2017	1.9	1.52	79	32.9	1.82	66.8	0.0807	1.46
5	7/12/2017	1.75	1.44	56	27.3	1.73	54.2	0.0214	0.17
6	8/1/2017	1.56	1.25	36	17.8	1.52	34	0.0324	0.406
7	8/17/2017	1.64	1.3	44	20	1.58	38.6	0.064	0.986
8	9/5/2017	1.65	1.37	45	23.5	1.66	46	-0.00205	-0.17
9	11/14/2017	1.45	1.16	28	14.6	1.43	27.2	0.0195	0.0565
10	3/21/2018	1.43	1.21	27	16	1.47	30.2	-0.0411	-0.667
11	5/1/2018	1.6	1.4	40	25.4	1.69	50.1	-0.0902	-1.19
12	5/22/2018	1.76	1.6	58	40.3	1.91	83.4	-0.15	-1.46
13	6/2/2018	2.26	2.09	180	122	2.45	284	-0.191	-1.93
14	7/18/2018	3	2.6	1010	395	3.01	1030	-0.00278	-0.286
15	9/6/2018	3.03	2.57	1060	373	2.98	973	0.0448	0.667
16	12/3/2018	2.65	2.35	449	226	2.74	559	-0.088	-0.986
17	2/26/2019	2.43	2.14	269	137	2.5	321	-0.0697	-0.816
18	3/14/2019	3.51	3.02	3260	1040	3.47	3010	0.0428	0.532
19	4/10/2019	2.2	1.87	157	74.8	2.21	165	-0.0144	-0.406
20	4/29/2019	3.51	3	3270	1000	3.45	2890	0.0605	0.816
21	6/11/2019	1.71	1.43	51	27.2	1.72	54	-0.0173	-0.532
22	10/8/2019	1.91	1.58	82	37.7	1.88	77.6	0.0314	0.286

Definitions

SSC: Suspended sediment concentration (SSC) in mg/L (80154) TBY: Turbidity in FNU (63680)

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